



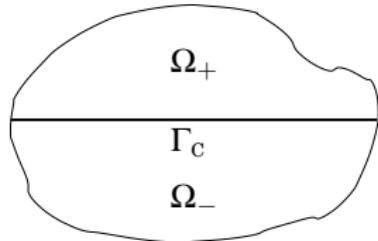
Weierstrass Institute for
Applied Analysis and Stochastics

A model for rate-independent, brittle delamination in thermo-visco-elasticity

joint work with Riccarda Rossi

Marita Thomas

Modeling of delamination along an interface

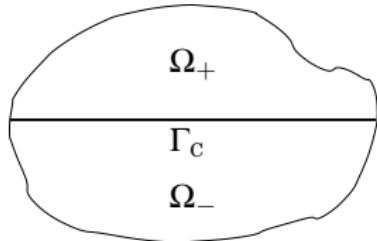


irreversible crack evolution along a prescribed surface

Γ_c : (flat) interface with evolving delamination
(= crack initiation & growth)

$$\Omega := \Omega_- \cup \Gamma_c \cup \Omega_+$$

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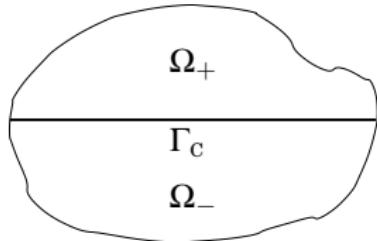
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Modeling approach: **Continuum damage mechanics**: [Frémond82,87]

delamination variable $z : [0, T] \times \Gamma_c \rightarrow [0, 1]$ volume fraction of **active** bonds

$$\text{crack}(t) := \{x \in \Gamma_c, z(t, x) = 0\} \quad \forall t_1 < t_2 : z(t_2) \leq z(t_1) \text{ a.e. on } \Gamma_c$$

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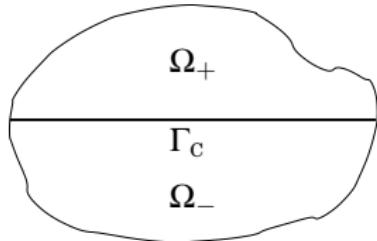
displacement $u : [0, T] \times \Omega$, $\llbracket u \rrbracket$: jump of u across Γ_c

brittle delamination: $\forall t \in [0, T] : z(t) \llbracket u(t) \rrbracket = 0$ a.e. on Γ_c

adhesive contact: $\forall t \in [0, T] : \underbrace{z(t) \llbracket u(t) \rrbracket \neq 0}_{\text{penalized by energy term}}$ allowed on Γ_c

[Kočvara/Mielke/Roubíček06, Roubíček/Scardia/Zanini09, Bonetti/Bonfanti/Rossi08,09]

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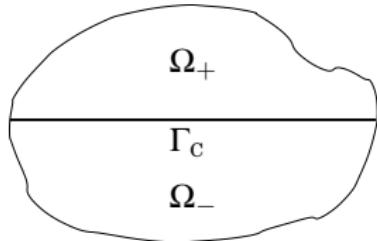
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Plan of the talk:

1. Mathematical modeling of delamination
 - Fully rate-independent evolution of brittle delamination:
energetic formulation
 - Extension of the model by rate-dependent effects
2. Adapted energetic formulation & suitable regularizations
3. Main result & mathematical tools

Rate-independent evolution of brittle delamination

State variable $q = (u, z)$:

$$u : [0, T] \times \Omega \rightarrow \mathbb{R}^d \quad \text{displacement}, e(u) = \frac{1}{2}(\nabla u + \nabla u^\top) \quad \text{lin. strain}$$
$$z : [0, T] \times \Gamma_C \rightarrow [0, 1] \quad \text{delamination variable}$$

Energy functional

$$\Phi(t, q) := \int_{\Omega \setminus \Gamma_C} W(e(u)) dx + \int_{\Gamma_C} (\mathcal{I}_{\{z[u]=0\}}([u], z) + I_{[0,1]}(z) + I_{\{[u] \cdot n \geq 0\}}([u]) - a_0 z) ds - \langle F(t), u \rangle$$

indicator function of set/constraint C : $I_C(y) := \begin{cases} 0 & \text{if } y \in C \\ \infty & \text{otherwise} \end{cases}$

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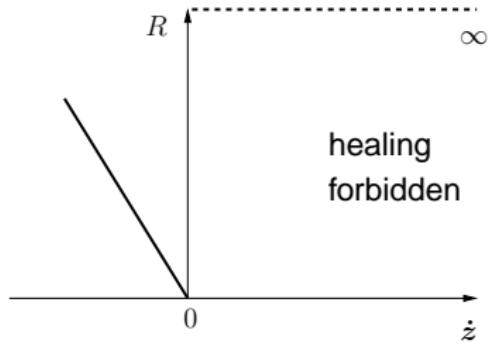
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Dissipation potential:

$$\mathcal{R}_1(\dot{z}) = \int_{\Gamma_C} R_1(\dot{z}(x)) ds \quad R_1(\dot{z}) := \begin{cases} a_1 |\dot{z}| & \text{if } \dot{z} \leq 0 \\ \infty & \text{else} \end{cases} \quad \text{with } a_1 > 0$$



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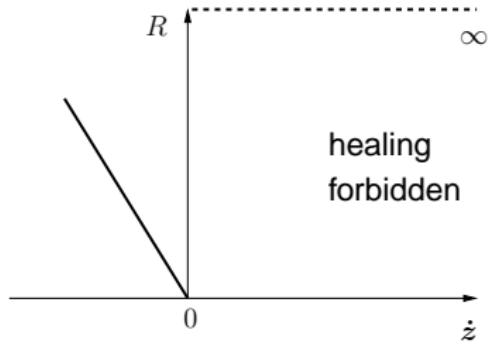
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Rate-independence \Leftrightarrow 1-homogeneity:

$$\mathcal{R}_1(0) = 0 \text{ and } \forall \lambda > 0 \forall v : \mathcal{R}_1(\lambda v) = \lambda \mathcal{R}_1(v)$$



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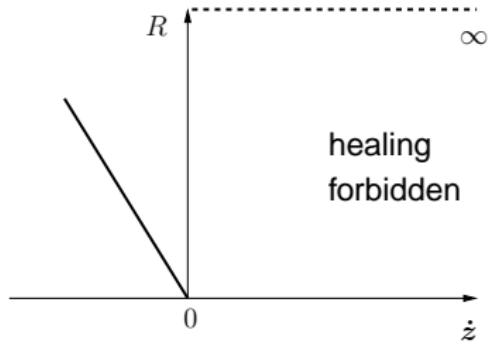
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Dissipation distance: $\mathcal{D}_1(z_1, z_2) = \mathcal{R}_1(z_2 - z_1)$



Rate-independent evolution of brittle delamination II

Subdifferential formulation:

$$\text{Find } q \in \mathcal{Q} \text{ such that } q(0) = q_0 \text{ and } 0 \in \partial_q \Phi(t, q) + \partial_{\dot{q}} \mathcal{R}_1(\dot{q})$$

Rate-independent evolution of brittle delamination II

Subdifferential formulation:

$$\text{Find } q \in \mathcal{Q} \text{ such that } q(0) = q_0 \text{ and } 0 \in \partial_q \Phi(t, q) + \partial_{\dot{q}} \mathcal{R}_1(\dot{q})$$

refers to the system (formally):

momentum balance for u in $(0, T) \times \Omega \setminus \Gamma_c$:

$$-\operatorname{div} D_e W(e(u)) = F \quad + \text{BCs on } (0, T) \times \partial\Omega + \text{IC}$$

& flow rule for z on $(0, T) \times \Gamma_c$:

$$0 \in \partial_z R_1(\dot{z}) + \partial_z I_{\{z[\![u]\!]=0\}}([\![u]\!], z) + \partial_z I_{[0,1]}(z) - a_0 \quad + \text{IC}$$

& constraint for (u, z) on $(0, T) \times \Gamma_c$:

$$[\![D_e W(e(u))]\!] n = 0$$

$$0 \in \partial_u I_{[z[\![u]\!]=0]}([\![u]\!], z) + \partial_u I_{[\![u]\!].n \geq 0}([\![u]\!]) + D_e W(e(u)) n$$

due to **brittle** constraint and **nonpenetration**

Subdifferential formulation:

$$\text{Find } q : [0, T] \rightarrow \mathcal{Q} \text{ such that } q(0) = q_0 \text{ and } 0 \in \partial_q \Phi(t, q) + \partial_{\dot{q}} \mathcal{R}_1(\dot{q})$$

Alternative, weaker problem formulation due to 1-homogeneity of \mathcal{R}_1

Find an **energetic solution** for $(\mathcal{Q}, \Phi, \mathcal{R}_1)$

Definition [Mielke&Co]: $q : [0, T] \rightarrow \mathcal{Q}$ is an **energetic solution** to $(\mathcal{Q}, \Phi, \mathcal{R}_1)$, if for all $t \in [0, T]$ it holds $\partial_t \Phi(\cdot, q(\cdot)) \in L^1((0, T))$, $\Phi(t, q(t)) < \infty$ and:

$$\begin{cases} (\text{S}) \text{ Stability: for all } \tilde{q} \in \mathcal{Q}: \Phi(t, q(t)) \leq \Phi(t, \tilde{q}) + \mathcal{R}_1(\tilde{z} - z(t)), \\ (\text{E}) \text{ Energy balance: } \Phi(t, q(t)) + \text{Diss}_{\mathcal{R}_1}(z, [0, t]) = \Phi(0, q(0)) + \int_0^t \partial_t \Phi(\xi, q(\xi)) d\xi, \end{cases}$$

$$\text{where } \text{Diss}_{\mathcal{R}_1}(z, [s, t]) := \sup_{\text{all part. of } [s, t]} \sum_{j=1}^N \mathcal{R}_1(z(\xi_j) - z(\xi_{j-1})).$$

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[Roubíček/Scardia/Zanini09]: Existence of energetic solutions for brittle delamination by approximation with adhesive contact: $\frac{k}{2} z |[\![u]\!]|^2 \rightarrow I_{\{z|[\![u]\!|=0\}}([\![u]\!], z)$ as $k \rightarrow \infty$!

Extention of the model:

brittle, **rate-independent** delamination & nonpenetration
& visco-elastic material & thermal effects

Analogous strategy as in the fully rate-independent case:

adhesive model from [Rossi/Roubíček10] $\xrightarrow{?}$ **brittle** model

Brittle delamination & nonpenetration

state variables: $u : [0, T] \times \Omega \rightarrow \mathbb{R}^d$ displacement, $e(u) = \frac{1}{2}(\nabla u + \nabla u^\top)$ lin. strain
 $z : [0, T] \times \Gamma_c \rightarrow \{0, 1\}$ delamination variable

(u, z) coupled in system given by

momentum balance($e(u)$)
& flow rule(\dot{z})
& constraint($z, [u]$) on Γ_c
due to brittle constraint & nonpenetration
+ BCs + ICs

rate-independent evolution of z

\Rightarrow energetic formulation via global stability & energy balance

Brittle delamination & nonpenetration & viscosity & therm. effects

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 $\theta : [0, T] \times \Omega \rightarrow (0, \infty)$ absolute temperature

(u, z, θ) coupled in system given by

momentum balance($e(u), e(\dot{u}), \theta$)
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rate-independent evolution of z but viscous evolution of u : $R_2(e(\dot{u})) = |e(\dot{u})|^2$,
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But: adapted energetic formulation of system in terms of 4 conditions [Roubíček10]:

1. weak momentum balance (for u)
2. weak enthalpy (in)equality (for θ)
3. semistability (for z)
4. mechanical energy 'balance'

adhesive model from [Rossi/Roubíček10]  brittle model

2. Adapted energetic formulation & sufficiently **regularized** models

3. Main result and tools

Weak formulation of the heat equation $(e(u), e(\dot{u}), \dot{\theta}, \theta)$

$$c_v(\theta) \dot{\theta} + \operatorname{div} \mathbb{J}(e(u), \theta) = 2R_2(e(\dot{u})) - \theta \mathbb{C} \mathbb{E} e(\dot{u}) + H \quad \text{in } [0, T] \times \Omega \setminus \Gamma_c$$

- H external heat source, \mathbb{C}, \mathbb{E} sym., pos. def. fourth order tensors
- Fourier's law for heat flux: $\mathbb{J}(e, \theta) = -\mathbb{K}(e, \theta) \nabla \theta$
- heat capacity $c_v(\theta)$
- viscous dissipation: $R_2(\dot{e}) := |\dot{e}|^2$

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Idea: Use time-discretization to prove existence of energetic sol.s for the full PDE-system

Problem: nonlinearity $c_v(\theta) \dot{\theta}$

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Way out: enthalpy-transformation [Roubíček10]:

$$\text{enthalpy } w = w(\theta) := \int_0^\theta c_v(\xi) d\xi, \quad \theta = \Theta(w), \quad \tilde{\mathbb{K}}(e, w) = \mathbb{K}(e, \Theta(w)) / c_v(\Theta(w)).$$

Reformulate full PDE-system in terms of w

Weak formulation of the heat equation $(e(u), e(\dot{u}), \dot{\theta}, \theta)$

$$\dot{w} - \operatorname{div}(\tilde{\mathbb{K}}(e(u), w) \nabla w) = 2R_2(e(\dot{u})) - \Theta(w) \mathbb{C} \mathbb{E} e(\dot{u}) + H \quad \text{in } [0, T] \times \Omega \setminus \Gamma_C$$

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 - viscous dissipation: $R_2(\dot{e}) := |\dot{e}|^2$
- + BCs on $\partial\Omega$ + conditions on Γ_C involving dissipation $R_1(\dot{z})$

leads to **weak enthalpy (in)equality**:

$$\begin{aligned} & \langle \zeta(T), w(T) \rangle + \int_Q \tilde{\mathbb{J}}(e(u), w) \cdot \nabla \zeta - w \dot{\zeta} \, dxdt + \int_{\Sigma_C} \eta([u], z) [\Theta(w)] [\zeta] \, dsdt \\ & \left\{ \begin{array}{l} = \\ \geq \end{array} \right\} \int_Q (2R_2(e(\dot{u})) \zeta - \Theta(w) \mathbb{C} \mathbb{E} : e(\dot{u}) \zeta) \, xdt + \int_{\Sigma_C} \frac{1}{2} (\zeta|_{\Gamma_C}^+ - \zeta|_{\Gamma_C}^-) d\xi_z^S(s, T) \\ & \quad + \int_Q H \zeta \, dxdt + \int_{\Omega \setminus \Gamma_C} w_0 \zeta(0) \, dx \end{aligned}$$

for all testfcts $\zeta \geq 0$ a.e.

adhesive contact '=' , brittle delamination ' \geq '

$d\xi_z^S(s, T)$ is a measure induced by dissipation $R_1(\dot{z})$

Weak formulation of the momentum balance $(e(u), e(\dot{u}), \theta)$

$$-\operatorname{div} \sigma(u, \dot{u}, \theta) = F \quad \text{in } [0, T] \times \Omega \setminus \Gamma_C \quad (F \text{ applied bulk force})$$

stress $\sigma(u, \dot{u}, \theta)$ features **viscous** response and **thermal effects** (Kelvin-Voigt rheology)

$$\sigma(u, \dot{u}, \theta) := D_e R_2(e(\dot{u})) + D_e W_p(e(u)) + C(e(u) - E\theta)$$

viscous dissipation: $R_2(\dot{e}) := |\dot{e}|^2$

bulk energy density: $W(e, \theta) := W_p(e) + \frac{1}{2}(e(u) - E\theta) : C : (e(u) - E\theta)$

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+ BCs + constraint($z, [\![u]\!]$) on Γ_C :

$$0 \in \partial_u I_{\{[\![u]\!] \cdot n \geq 0\}}(u) + \sigma(u, \dot{u}, \theta)n + \partial_u I_{\{z[\![u]\!] = 0\}}(z, u)$$

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+ BCs + constraint $(z, [\![u]\!])$ on Γ_C :

$$0 \in \partial_u I_{\{[\![u]\!] \cdot n \geq 0\}}(u) + \sigma(u, \dot{u}, \theta)n + \partial_u I_{\{z[\![u]\!] = 0\}}(z, u)$$

leads to weak momentum balance as a variational inequality for a.a. $t \in (0, T)$:

$[\![u(t)]!] \cdot n \geq 0$, $z(t)[\![u(t)]!] = 0$ on Γ_C and

$$\begin{aligned} \int_{\Omega \setminus \Gamma_C} (D_e W(e(u(t)), \Theta(w(t))) + D_e R_2(e(\dot{u}(t)))) : e(v - u(t)) dx \\ \geq \int_{\Omega \setminus \Gamma_C} F(t) \cdot (v - u(t)) dx \end{aligned}$$

for all sufficiently smooth testfct.s v with $[\![v]\!] \cdot n \geq 0$ and $z(t)[\![v]\!] = 0$ on Γ_C

Weak formulation of the momentum balance $(e(u), e(\dot{u}), \theta)$

$$-\operatorname{div} \sigma(u, \dot{u}, \theta) = F \quad \text{in } [0, T] \times \Omega \setminus \Gamma_C$$

stress $\sigma(u, \dot{u}, \theta)$ features viscous response and thermal effects (Kelvin-Voigt rheology)

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double constraint \Rightarrow approximate brittle constraint $z(t)[\![v]\!] = 0$ by adhesive contact

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approximate brittle constraint $z(t)[\![v]\!] = 0$ by adhesive contact

$$0 \in \partial_{\dot{z}} R_1(\dot{z}) + \partial_z \phi^s(z, [\![u]\!]) \quad \text{on } \Gamma_C$$

- rate-independent dissipation $R_1(\dot{z}) = -a_1 \dot{z} + I_{(-\infty, 0]}(\dot{z})$
- surface energy density $\phi^s(z, [\![u]\!]) = -a_0 z + I_{[0, 1]}(z) + I_{[z[\![u]\!]=0]}(z, [\![u]\!])$

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weak formulation: semistability

$$\forall t \in [0, T], \forall \text{ testfcts } \tilde{z}: \quad \Phi^s(z(t), [\![u(t)]\!]) \leq \Phi^s(\tilde{z}, [\![u(t)]\!]) + \mathcal{R}_1(\tilde{z} - z(t))$$

'partial' stability condition, since $u(t)$ (energetic sol.) is fixed!

Recall stability in the (fully) rate-independent setting:

$$\forall t \in [0, T], \forall \text{ testfcts } (\tilde{u}, \tilde{z}): \quad \mathcal{E}(t, u(t), z(t)) \leq \mathcal{E}(t, \tilde{u}, \tilde{z}) + \mathcal{R}_1(\tilde{z} - z(t))$$

Weak formulation of the flow rule(\dot{z}) & regularizations

$$\forall t \in [0, T], \forall \text{ testfcts } \tilde{z}: \quad \Phi^s(z(t), \llbracket u(t) \rrbracket) \leq \Phi^s(\tilde{z}, \llbracket u(t) \rrbracket) + \mathcal{R}_1(\tilde{z} - z(t))$$

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Regularizations:

1. adhesive contact: $\phi^s(z, [\![u]\!]) = -a_0 z + I_{[0,1]}(z) + \frac{k}{2} z |[\![u]\!]|^2$

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2. enforce $z \in \{0, 1\}$ \rightsquigarrow suitable setting:

$\text{SBV}(\Gamma_c, \{0, 1\}) := \{z: \Gamma_c \rightarrow \{0, 1\}, z \text{ characteristic fct. of set } Z \subset \Gamma_c \text{ with } P(Z, \Gamma_c) < \infty\}$

$$\Phi^s(z, [\![u]\!]) + \mathcal{G}_b(z)$$

$\mathcal{G}_b(z) := bP(Z, \Gamma_c)$ perimeter of Z (= total variation of z)



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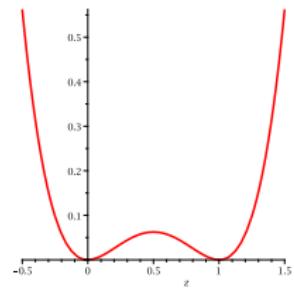
$\mathcal{G}_b(z) := bP(Z, \Gamma_c)$ perimeter of Z (= total variation of z)

3. Modica-Mortola approximation:

$$\mathcal{G}_m(z) := \begin{cases} \int_{\Gamma_c} (m^2 z^2 (1-z)^2 + \frac{1}{m^2} |\nabla z|^2) dx & \text{if } z \in H^1(\Omega, [0, 1]) \\ \infty & \text{otherwise} \end{cases}$$

$\mathcal{G}_m \xrightarrow{\Gamma} \mathcal{G}_b$ as $m \rightarrow \infty$

[Giacomini05] Volume damage \rightarrow Francfort-Marigo crack model



Weak formulation of the flow rule(\dot{z}) & regularizations

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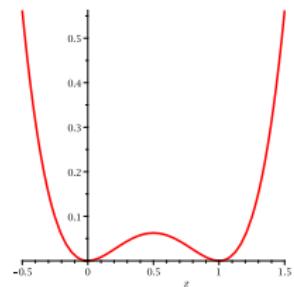
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$\mathcal{G}_m \xrightarrow{\Gamma} \mathcal{G}_b$ as $m \rightarrow \infty$ adapted to stability cond. for unidirectional \mathcal{R}_1 : [Th11]



Mechanical energy 'balance'

Energy terms:

- mechanical energy $\Phi(u, z) = \Phi^{\text{bulk}}(u, z) + \Phi^{\text{surf}}(z, \llbracket u \rrbracket)$
- mechanical bulk energy $\Phi^{\text{bulk}}(u, z) = \int_{\Omega \setminus \Gamma_C} W_p(e(u)) + \frac{1}{2} e(u) : C : e(u) \, dx$
- mechanical surface energy

$$\Phi^{\text{surf}}(z, \llbracket u \rrbracket) := \int_{\Gamma_C} (-a_0 z + I_{[0,1]}(z) + J_k(z, \llbracket u \rrbracket) + I_{\{\llbracket u \rrbracket \cdot n \geq 0\}}(\llbracket u \rrbracket)) \, ds + \mathcal{G}(z)$$

$$J_k(z, \llbracket u \rrbracket) = \begin{cases} \frac{k}{2} z |\llbracket u \rrbracket|^2 & \text{adhesive, } k \in \mathbb{N} \\ I_{\{z \llbracket u \rrbracket = 0\}}(z, \llbracket u \rrbracket) & \text{brittle, } k = \infty \end{cases}$$

$$\mathcal{G}(z) = \begin{cases} \mathcal{G}_m(z) & \text{Modica-Mortola} \\ \mathcal{G}_b(z) & \text{SBV (perimeter)} \end{cases}$$

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Mechanical energy 'balance' for a.a. $t \in (0, T)$:

$$\Phi(u(t), z(t)) + \int_0^t \int_{\Omega \setminus \Gamma_C} 2R_2(e(\dot{u})) \, dx \, d\xi + \mathcal{R}_1(z(t) - z(0))$$
$$\left\{ \begin{array}{c} = \\ \leq \end{array} \right\} \Phi(u(0), z(0)) + \int_0^t \int_{\Omega \setminus \Gamma_C} \Theta(w) \mathbb{C} \mathbb{E} : e(\dot{u}) \, dx \, d\xi + \int_0^t \int_{\Omega \setminus \Gamma_C} F(t) \cdot \dot{u} \, dx \, d\xi$$

3. Results: Approximation procedure (viscous, θ -dependent setting)

$$\Phi_{km}^{\text{surf}}(z, [\![u]\!]) := \int_{\Gamma_C} (-a_0 z + I_{[0,1]}(z) + I_{\{[\![u]\!]\cdot n \geq 0\}}([\![u]\!]) + \frac{k}{2} z |[\![u]\!]|^2) \, ds + \mathcal{G}_m(z)$$

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Limit passage:

Modica-Mortola **adhesive** contact \rightarrow **SBV-adhesive** contact

Theorem: Keep $k \in \mathbb{N}$ fixed & assumptions on given data. As $m \rightarrow \infty$, (a subsequence of) the energetic solutions of the Modica-Mortola **adhesive** contact models approximate an energetic solution of the **SBV-adhesive** contact model.

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Limit passage $k \rightarrow \infty$:

SBV-adhesive contact \rightarrow **SBV-brittle** delamination

Main result: Limit passage SBV-adhesive contact → SBV-brittle delamination

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Main difficulty: Limit passage in weak momentum balance!

weak momentum balance for SBV-adhesive delamination f.a.a. $t \in (0, T)$:

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$$+ \overbrace{\int_{\Gamma_C} k z_k(t) [u_k(t)] \cdot [v - u_k(t)] ds}^{\text{cross term}}$$

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$$\int_{\Omega \setminus \Gamma_C} (D_e W(e(u_k(t)), \Theta(w_k(t))) + D_e R_2(e(\dot{u}_k(t)))) : e(v_k - u_k(t)) dx$$

$$+ \cancel{\int_{\Gamma_C} kz_k(t)[u_k(t)] \cdot [v_k - u_k(t)] ds}$$

$$\geq + \int_Q F(t) \cdot (v_k - u_k(t)) dx$$

for all sufficiently smooth testfct.s v_k with $[v_k] \cdot n \geq 0$ and $z_k(t)[v_k] = 0$ on Γ_C

Reason for $v_k \rightarrow v$ strongly in $W^{1,p}$: Mosco-conv. of energy fct. \Rightarrow G-conv. of derivative

Recovery sequence & support property

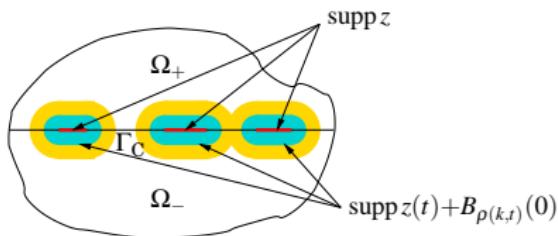
For given testfct. v construct recovery sequence $(v_k)_{k \in \mathbb{N}}$ such that

$$\forall k \in \mathbb{N}: \int_{\Sigma_C} kz_k \llbracket u_k \rrbracket \cdot \llbracket v_k \rrbracket = 0$$

and $v_k(t) \rightarrow v(t)$ strongly in $W^{1,p}(\Omega \setminus \Gamma_C, \mathbb{R}^d)$

Tool: Support convergence: $\forall t \in [0, T]$

$$\text{supp } z_k(t) \subset \text{supp } z(t) + B_{\rho(k,t)}(0) \text{ for all } k \in \mathbb{N} \text{ and } \rho(k,t) \rightarrow 0 \text{ as } k \rightarrow \infty$$



$v_k(t) \in W^{1,p}(\Omega \setminus \Gamma_C, \mathbb{R}^d)$ s.th.
 $v_k(t) = 0$ in $\text{supp } z(t) + B_{\rho(k,t)}(0)$,
 $v_k(t) = v(t)$ in $\Omega \setminus \text{supp } z(t) + B_{2\rho(k,t)}(0)$
 $\llbracket v_k(t) \rrbracket \cdot n \geq 0$ on Γ_C

[Mielke/Roubíček/Th10]: Let $p > d$. Then, $v_k(t) \rightarrow v(t)$ strongly in $W^{1,p}(\Omega \setminus \Gamma_C, \mathbb{R}^d)$.

([Lewis88]: Hardy's inequality)

Support convergence

Support convergence: $\forall t \in [0, T]$

$\text{supp } z_k(t) \subset \text{supp } z(t) + B_{\rho(k,t)(0)}$ for all $k \in \mathbb{N}$ and $\rho(k,t) \rightarrow 0$ as $k \rightarrow \infty$

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$$\mathcal{L}^{d-1}((\text{supp } z \setminus \text{supp } z_k) \cup (\text{supp } z_k \setminus \text{supp } z)) \rightarrow 0$$

Support convergence

Support convergence: $\forall t \in [0, T]$

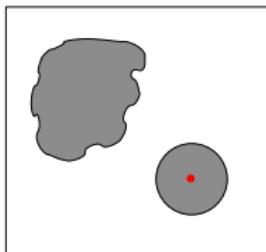
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Not sufficient for support convergence:



Support convergence

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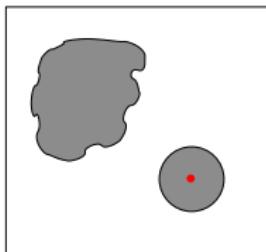
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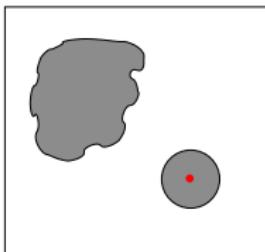
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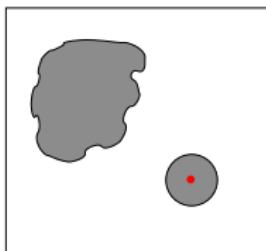
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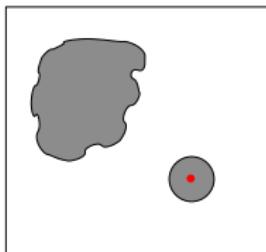
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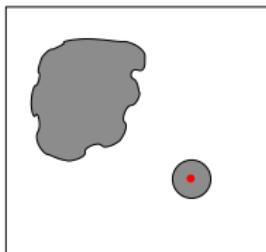
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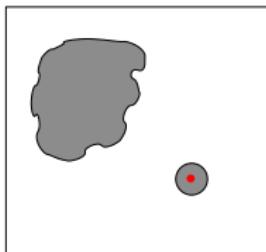
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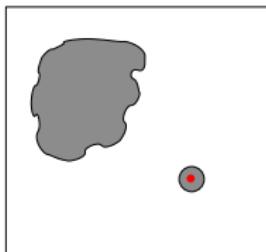
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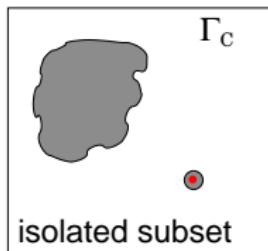
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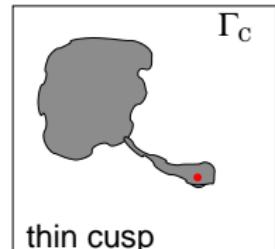
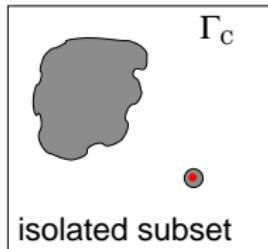
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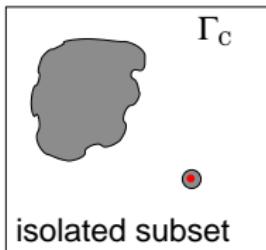
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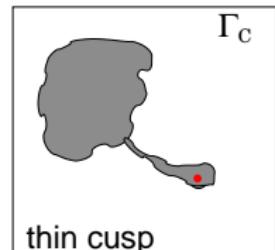
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Exclude arbitrarily small sets by semistability!



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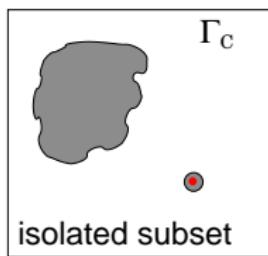
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$$\Phi_k(z_k, [\![u_k]\!]) = \int_{\Gamma_c} (-a_0 z_k + \frac{k}{2} z_k |[\![u_k]\!]|^2) \, ds + bP(Z_k, [\![u_k]\!])$$



Exclude arbitrarily small sets by semistability!

z_k semistable charact. fct. of Z_k , $A \subset Z_k$ isolated

test semistability with \tilde{z} charact. fct. of $Z_k \setminus A$:

$$\Phi_k(z_k, [\![u_k]\!]) \leq \Phi_k(\tilde{z}, [\![u_k]\!]) + \mathcal{R}_1(\tilde{z} - z_k)$$

$$\Rightarrow bP(A, \Gamma_c) \leq (a_0 + a_1) \mathcal{L}^{d-1}(A)$$

$$\frac{b}{(a_0 + a_1)} \leq \frac{\mathcal{L}^{d-1}(A)}{P(A, \Gamma_c)} \leq c_{d-1} \mathcal{L}^{d-1}(A)^{1/(d-1)}$$

isoperimetric inequality

R. ROSSI AND M. THOMAS:

From an adhesive to a brittle delamination model in thermo-visco-elasticity,
WIAS-Preprint 1692.

Thank You!